

26566

On the anisotropy of the elastic ... S/126/61/012/002/018/019
E032/E514

the anisotropy may also be due to the fact that the thermal expansion coefficient is not the same in all directions. However, according to A. M. Belikov (Ref.10: Dissertation, MIS, 1958) the expansion coefficient along the a and c axes is in fact practically the same (3.84×10^{-6} and 3.90×10^{-6}). There are 1 table and 10 references: 7 Soviet and 3 non-Soviet.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut
tverdykh splavov (All Union Scientific Research
Institute for Hard Alloys)

SUBMITTED: March 11, 1961

Card 3/3

ACCESSION NR: AP4015266

S/0226/64/000/001/0056/0064

AUTHORS: Ivensen, V. A.; Eyduk, O. N.

TITLE: The structure of two-phase solid cermet alloys

SOURCE: Poroshkovaya metallurgiya, no. 1, 1964, 56-64

TOPIC TAGS: WC Co alloy, carbide phase structure, cobalt phase structure, binary cermet alloy, cermet, Co phase microscopic analysis, WC phase microscopic analysis

ABSTRACT: A discussion concerning the structure of WC-Co alloys is presented. It starts with a short review of the opinions expressed by other authors and a criticism of their conclusions. According to previous investigations, the analyses made with electron microscope showed that the carbide phase appeared to be continuous while the cobalt phase was concentrated in the inclusions, seemingly isolated from each other. However, this isolation was observed only in the polished sections. On the other hand, the fact that cobalt was removed from the alloy by the action of hydrochloric acid pointed to the existence of connections between the isolated cobalt areas. The authors believe that the degree of carbide grain coalescence depends on the differences in the technical process involved, and they claim that the cobalt "interlayers" between the carbide grains

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ACCESSION NR: APL015266

affect the physical nature of the material. It is concluded that the degree of carbide grain coalescence should be regarded as a very important structural characteristic of the alloy studied and that it should be accounted for (together with such other structural characteristics as the grain size, etc) in determining the physical properties of the WC-Co alloy. Orig. art. has: 7 photographs.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov, Moscow (All-Union Scientific Research Institute of Hard Alloys)

SUBMITTED: 13Feb64

DATE ACQ: 12Mar64

ENCL: 00

SUB CODE: ML

NO REF SOV: 009

OTHER: 008

Card 2/2

ACCESSION NR: AP4044910

S/0226/64/000/004/0043/0057

AUTHOR: Ivensen, V.A., Eyduk, O.N., Pivovarov, L.Kh.

TITLE: Some regularities in the deformation of sintered hard alloys of WC-Co

SOURCE: Poroshkovaya metallurgiya, no. 4, 1964, 43-57

TOPIC TAGS: sintered alloy, powder alloy, tungsten carbide, hard alloy, cobalt alloy, tungsten carbide alloy, alloy deformation, plastic deformation, alloy structure, yield point

ABSTRACT: It has recently been established that there is no direct relationship between the bending strength of a hard alloy and its notch toughness, and this fact has attracted interest to phenomena connected with the deformation of hard alloys. However, the relative deformations of the cobalt and the carbide phases and their separate roles in the total deformation process have not yet been clarified. In order to fill this gap, the present authors investigated the hard alloy WC-Co with respect to plastic deformation and its dependence on the composition (6-50% Co) and structure (fine grain and coarse grain). Prismatic test specimens (10x10x20 mm) of the hard alloy were deformed under the influence of gradually increasing uniaxial compressive loads. The residual

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ACCESSION NR: AP4044910

deformation was measured by an optimeter and the yield point was determined from logarithmic stress-strain curves, corresponding to a permanent strain of 0.1%. The lateral faces of the specimens were ground and polished before the tests, and some of the specimens were subjected to X-ray investigations before and after deformation. Such specimens were annealed at 800C before deformation to remove the strain-hardening effect produced by the grinding. The width of the radiospectrographic lines was measured by the ionization method. Grain size and angle of disorientation were computed from the number and size of the reflexes obtained photographically. These studies revealed plastic deformation of the tungsten carbide grains, as indicated by numerous bands of slippage appearing on the surface of the grains after deformation, as well as by an increase in the number of reflexes on the X-ray picture. The yield point of the hard alloy was found to be directly proportional to the relative value of the contact surface of the tungsten carbide grains. The resistance to deformation of the alloy in the initial stages is determined mainly by the resistance to deformation of the carbide skeleton. It is only after further deformation that the resistance to deformation of the strain-hardened cobalt phase is manifested. The mechanism of deformation of the carbide skeleton of the alloy does not differ in principle from that of a polycrystalline

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ACCESSION NR: AP4044910

metal. Orig. art. has: 4 graphs, 15 photomicrographs and 6 tables.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov
(All-Union Scientific Research Institute of Hard Alloys)

SUBMITTED: 15Aug63

ENCL: 00

SUB CODE: MM

NO REF SOV: 003

OTHER: 006

3/3

Cord

L 20667-66 ENT(d)/ENT(m)/EMP(w)/T/EMP(t)/EMP(k) IJP(n) JD/HW/EM

ACC NR: AP6001477

SOURCE CODE: UR/0226/65/000/012/0069/0072

AUTHOR: Ivensen, V. A.; Gol'dberg, Z. A.; Eyduk, O. N.; Fal'kovskiy, V. A. ⁵⁵ 13

ORG: All-Union Scientific Research Institute of Hard Alloys (Vsesoyuzhnyy nauchno-issledovatel'skiy institut tverdykh splavov)

TITLE: Resistance of a hard alloy to failure under impact loads

SOURCE: Poroshkovaya metallurgiya, no. 12, 1965, 69-72

TOPIC TAGS: plastic deformation, mechanical shock resistance, specific resistance, compressive strength, ultimate stress, bending stress, data analysis, tungsten containing alloy, failure

ABSTRACT: The effect of plastic deformation of a hard alloy on its resistance to failure under impact loads was analyzed. It was shown that despite the relatively low value of plastic deformation, the latter has a great effect on the efficiency of the hard-alloy load. This was corroborated by experimental data characterizing the efficiency of a very coarse-grained and a medium-grained alloy with 20% Co. The resistance to failure and efficiency of the coarse-grained alloy is much greater than that of the medium-grained alloy despite the higher ultimate bending and compression strengths of the latter. The differ-

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L 20667-66

ACC NR: AP6001477

ence in tool efficiency is explained by the greater deformability of
the coarse-grained alloy. Orig. art. has: 1 table. [Based on author's
abstract] [NT]

SUB CODE: 11, 20/ SUBM DATE: 13Feb65/ ORIG REF: 003/ OTH REF: 001

Card

2/2

BK

ABELEV, Yu.M.; BRAYT, P.I.; KRUTOV, V.I.; KULACHENOK, B.G.; SOROCHAN,
Ye.A.; EYDOK, R.P.

Testing a series 1-480-P large-panel apartment house erected on
settling soil. Osn., fund.i mekh.grun. 4 no.2:3-5 '62.
(MIRA 15:8)

(Zaporozh'ye—Apartment houses—Testing)

ABELEV, Yuriy Mordukhovich, doktor tekhn. nauk; KRUTOV, Vladimir Ivanovich, kand. tekhn. nauk; EYDUK, Rudol'f Petrovich, st. nauchn. sotr., inzh.; POLUBNEVA, V.I., inzh., nauchn. red.

[Preparation of foundation beds and the laying of foundations of large-panel apartment houses on sagging soil; practices of the Research Institute for Foundation Beds and Underground Structures of the State Committee on Construction of the Council of Ministers of the U.S.S.R. and of the Zaporozh'ye Housing Construction Trust, and the Nikopol' Construction Foundations Trust] Podgotovka osnovanii i ustroistvo fundamentov krupnopanel'nykh zhilykh domov na prosadochnykh gruntakh; iz opyta NII osnovanii i podzemnykh sooruzhenii Gosstroia SSSR, trestov "Zaporozhzhilstroi" i "Nikopol'stoi." Moskva, Stroiizdat, 1965. 19 p. (MIRA 18:9)

1. Rukovoditel' laboratorii stroitel'stva na prosadochnykh gruntakh Nauchno-issledovatel'skogo instituta osnovaniy i podzemnykh sooruzhenii (for Abelev). 2. Laboratoriya stroitel'stva na posadochnykh gruntakh Nauchno-issledovatel'skogo instituta osnovaniy i podzemnykh sooruzhenii, Moskva (for Krutov, Eyduk).

CO

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PROCESSES AND PROPERTIES INDEX

A rapid method for determination of the purity of technical gypsum. J. Biduks, *Acta Univ. Latvianis, Kim. Fakultat. Ser. B*, 196, 1-4, 1-9 (in German 10)(1938).—The method depends upon the fact that a powder immersed in a liquid of similar n exhibits different degrees of color intensity, depending on the purity. Heat the gypsum to 450° or 500° to destroy org. matter. Mix the purest and least pure grades of gypsum in such proportions that the CaSO_4 content increases in steps of 1% and immerse the mint. in tech. benzene. Against the scale on constructed match the unknown for equal degree of darkness. The accuracy of the result is 1-2%. P. S. R.

Common Elements

Individual Metals

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

14-1088 14-1089 14-1090 14-1091 14-1092 14-1093 14-1094 14-1095 14-1096 14-1097 14-1098 14-1099 14-1100 14-1101 14-1102 14-1103 14-1104 14-1105 14-1106 14-1107 14-1108 14-1109 14-1110 14-1111 14-1112 14-1113 14-1114 14-1115 14-1116 14-1117 14-1118 14-1119 14-1120 14-1121 14-1122 14-1123 14-1124 14-1125 14-1126 14-1127 14-1128 14-1129 14-1130 14-1131 14-1132 14-1133 14-1134 14-1135 14-1136 14-1137 14-1138 14-1139 14-1140 14-1141 14-1142 14-1143 14-1144 14-1145 14-1146 14-1147 14-1148 14-1149 14-1150 14-1151 14-1152 14-1153 14-1154 14-1155 14-1156 14-1157 14-1158 14-1159 14-1160 14-1161 14-1162 14-1163 14-1164 14-1165 14-1166 14-1167 14-1168 14-1169 14-1170 14-1171 14-1172 14-1173 14-1174 14-1175 14-1176 14-1177 14-1178 14-1179 14-1180 14-1181 14-1182 14-1183 14-1184 14-1185 14-1186 14-1187 14-1188 14-1189 14-1190 14-1191 14-1192 14-1193 14-1194 14-1195 14-1196 14-1197 14-1198 14-1199 14-1200 14-1201 14-1202 14-1203 14-1204 14-1205 14-1206 14-1207 14-1208 14-1209 14-1210 14-1211 14-1212 14-1213 14-1214 14-1215 14-1216 14-1217 14-1218 14-1219 14-1220 14-1221 14-1222 14-1223 14-1224 14-1225 14-1226 14-1227 14-1228 14-1229 14-1230 14-1231 14-1232 14-1233 14-1234 14-1235 14-1236 14-1237 14-1238 14-1239 14-1240 14-1241 14-1242 14-1243 14-1244 14-1245 14-1246 14-1247 14-1248 14-1249 14-1250 14-1251 14-1252 14-1253 14-1254 14-1255 14-1256 14-1257 14-1258 14-1259 14-1260 14-1261 14-1262 14-1263 14-1264 14-1265 14-1266 14-1267 14-1268 14-1269 14-1270 14-1271 14-1272 14-1273 14-1274 14-1275 14-1276 14-1277 14-1278 14-1279 14-1280 14-1281 14-1282 14-1283 14-1284 14-1285 14-1286 14-1287 14-1288 14-1289 14-1290 14-1291 14-1292 14-1293 14-1294 14-1295 14-1296 14-1297 14-1298 14-1299 14-1300 14-1301 14-1302 14-1303 14-1304 14-1305 14-1306 14-1307 14-1308 14-1309 14-1310 14-1311 14-1312 14-1313 14-1314 14-1315 14-1316 14-1317 14-1318 14-1319 14-1320 14-1321 14-1322 14-1323 14-1324 14-1325 14-1326 14-1327 14-1328 14-1329 14-1330 14-1331 14-1332 14-1333 14-1334 14-1335 14-1336 14-1337 14-1338 14-1339 14-1340 14-1341 14-1342 14-1343 14-1344 14-1345 14-1346 14-1347 14-1348 14-1349 14-1350 14-1351 14-1352 14-1353 14-1354 14-1355 14-1356 14-1357 14-1358 14-1359 14-1360 14-1361 14-1362 14-1363 14-1364 14-1365 14-1366 14-1367 14-1368 14-1369 14-1370 14-1371 14-1372 14-1373 14-1374 14-1375 14-1376 14-1377 14-1378 14-1379 14-1380 14-1381 14-1382 14-1383 14-1384 14-1385 14-1386 14-1387 14-1388 14-1389 14-1390 14-1391 14-1392 14-1393 14-1394 14-1395 14-1396 14-1397 14-1398 14-1399 14-1400 14-1401 14-1402 14-1403 14-1404 14-1405 14-1406 14-1407 14-1408 14-1409 14-1410 14-1411 14-1412 14-1413 14-1414 14-1415 14-1416 14-1417 14-1418 14-1419 14-1420 14-1421 14-1422 14-1423 14-1424 14-1425 14-1426 14-1427 14-1428 14-1429 14-1430 14-1431 14-1432 14-1433 14-1434 14-1435 14-1436 14-1437 14-1438 14-1439 14-1440 14-1441 14-1442 14-1443 14-1444 14-1445 14-1446 14-1447 14-1448 14-1449 14-1450 14-1451 14-1452 14-1453 14-1454 14-1455 14-1456 14-1457 14-1458 14-1459 14-1460 14-1461 14-1462 14-1463 14-1464 14-1465 14-1466 14-1467 14-1468 14-1469 14-1470 14-1471 14-1472 14-1473 14-1474 14-1475 14-1476 14-1477 14-1478 14-1479 14-1480 14-1481 14-1482 14-1483 14-1484 14-1485 14-1486 14-1487 14-1488 14-1489 14-1490 14-1491 14-1492 14-1493 14-1494 14-1495 14-1496 14-1497 14-1498 14-1499 14-1500 14-1501 14-1502 14-1503 14-1504 14-1505 14-1506 14-1507 14-1508 14-1509 14-1510 14-1511 14-1512 14-1513 14-1514 14-1515 14-1516 14-1517 14-1518 14-1519 14-1520 14-1521 14-1522 14-1523 14-1524 14-1525 14-1526 14-1527 14-1528 14-1529 14-1530 14-1531 14-1532 14-1533 14-1534 14-1535 14-1536 14-1537 14-1538 14-1539 14-1540 14-1541 14-1542 14-1543 14-1544 14-1545 14-1546 14-1547 14-1548 14-1549 14-1550 14-1551 14-1552 14-1553 14-1554 14-1555 14-1556 14-1557 14-1558 14-1559 14-1560 14-1561 14-1562 14-1563 14-1564 14-1565 14-1566 14-1

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Latvian clays as raw materials for the preparation of clinker (ceramic bodies). J. Rikulis, *Acta Univ. Lat-
vianis, Kiv. Fakult. Ser. B*, 196, 1-4, 35-135 (in Ger-
man 126-41) (1936).—The clays belong to the Devonian
(D.), Tertiary (T.) and Quaternary (Q.). They contain
much Fe and alkalies, and also Ti. The max. contents
are, Fe_2O_3 12.4, K₂O and Na₂O 6.9, TiO_2 1.15 and Al₂O₃
23.4%. The alkalies in the D. clays are mostly in mica
and feldspar. More mica is present in the D. than in the
Q. clays. The D. clays melt at cones 8-14 and the Q. at
2-7. The addn. of fine sand is desirable. Specimens
burned in a reducing atm. are more sol. in acid than those
burned in an oxidizing atm. Decompn. of Fe_2O_3 to lower
oxides took place at 1100° and above. P. S. Koller

L 32244-65 EWT(d)/EWP(e)/EWT(m)/EWA(d)/EWP(v)/T/EWP(t)/EWP(k)/EWP(h)/EWP(b)/
EWP(1) Pf-4 IJP(c) JD/JG

ACCESSION NR: AR5004771

S/0137/64/000/010/G036/G036

SOURCE: Ref. zh. Metallurgiya, Abs. 100245

AUTHOR: Vodop'yanova, L. S.; Marychev, V. V.; Eyduk, Yu. A.

TITLE: Study of high temperature sintering of tungsten

CITED SOURCE: Sb. tr. Vses. n.-i. in-t tverdykh splavov, no. 5,
1964, 221-224

TOPIC TAGS: tungsten, powder metallurgy, powder metal pressing,
sintering, temperature dependence, impurity content, vacuum refining

TRANSLATION: Tungsten powder prepared by reduction of WO_3 was pressed on a hydraulic press under a pressure of 2 tons/cm². The resulting molded pieces, which had a low density, were first sintered in a hydrogen atmosphere at 750-800° (1-1.5 hrs). Final sintering of the molded pieces was done in a TsEP-302 vacuum welding machine under a vacuum of 10⁻³ mm Hg and a rate of temperature increase of 500°/min. The molded pieces began to sinter at 1300-1500°. The rate of sintering increased sharply when the temperature was

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ACCESSION NR: AR5004771

raised to 2400°. Further temperature increase was not accompanied by any significant increase in the density of the molded pieces. Silicon impurities (in the form of elemental silicon) and copper impurities were eliminated at 1300°, calcium, chromium, iron, and nickel impurities at 1600-1800°, and aluminum impurities at 2000-2200°. Oxygen was intensively eliminated at temperatures above 2200°. The oxygen content in tungsten sintered at 2200° did not exceed 0.005%. V. Neshpor.

SUB CODE: MM

ENCL: 00

Card 2/2

EYDUK, Yu.Ya.

EYDUK, Yu Ya. -- "Characteristics of Clays of the Latvian SSR and Their Suitability for Making Clinker Shapes." Latvian State U, 1949. In Latvian (Dissertation for the Degree of Candidate of Chemical Sciences)

SO: Izvestiya Ak. Nauk Latvviyskoy SSR, No. 9, Sept., 1955

IYEVII 'SH, A.F.[Ievinš, A.], glav. red.; EYDOK, Yu.Ya.[Eiduks, J.],
zam. glav. red.; VAYVAD, A.Ya.[Vaivads, A.], red.; KUKURS,
O.K., red.; MAKSIMOVA, O.S., red.; UPIE, A.Yu., red.;
DYMARSKAYA, O., red.

[Glazes, their production and application] Glazuri, ikh
proizvodstvo i primenenie. Riga, Izd-vo AN Latviiskoi SSR,
1964. 249 p. (MIRA 18:4)

1. Latvijas Padomju Socialistiskas Republikas Zinatnu
Akademija. Kimijas instituts.

EYDURS, Y.

SIDURS, J.; HOFMANIS, B.

Method for rapid determination of hydrate water in gypsum which contains dolomite. Latvijas PSR Zinatnu Akad. Vestis '49, No.7, 85-90. (MLRA 4:1) (CA 48 no.1:341 '54)

EIDUKS, Yu.

Brit Abs B1
June 1953

Building and road-
making materials

(5)
7mol

Use of gypsum quarry wastes as a source of bonding agents. Yu. Eiduks, A. Vaivels, A. Apinis, and B. Holman (*Kim. Inst. Zinatistis Raksti, Riga*, 1950, 1, 5-33).—The wastes contain 48-65% of $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$, 15-33% of dolomite, and 12-20% of clay; when heated to 170° they yield a second-grade plaster of Paris, and a product resembling anhydrite cement is obtained with optimum mechanical properties by calcination at $750-850^\circ$ with 1% of NaHSO_4 + 5% of CaO + 15% of open-hearth slag; it contains CaSO_4 with small quantities of $\text{CaO} \cdot \text{Al}_2\text{O}_3 + 2\text{CaO} \cdot \text{SiO}_2$.

EYDUKS, YU.

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Brit Abst. 51
June 1953
Building and
Road MAKING
Materials

Possibility of extending the range of Portland cements in the Latvian SSR. K. Karlson, Yu. Edduks, and A. Valvads (Kiev. Inst. Zinatniskie Raksti, Riga, 1950, 1, 171—188).—The conditions are established for obtaining high-grade Portland cement by firing at 1485° a mixture of clay from the Brotsensk district with lime, the coeff. of saturation of SiO_2 by CaO in the clinker being 0.94. In an attempt to find suitable pozzuolanic Portland cement mixtures, it is established that the most suitable "hydraulic" addition is clay from the Kengarag district, fired at 900°, since the cement produced with it is salt-resistant and stronger after storage in water for 180 days than plain Portland cement. The suitability of a fired clay for this purpose can be assessed from an analysis of the H_2O extract from it: <5% of the Al_2O_3 in the clay should be present. R. C. MURRAY.

EIDUKS, J.

Chemical Abstracts
Vol. 48 No. 5
Mar. 10, 1954
Cement, Concrete, and Other
Building Materials

Suitability of local (Latvian) dolomite and lime marls for the production of Roman cement. — J. Eiduks, A. Valvads, and V. Mjaskova (Acad. Sci. Latv., S.S.R., Riga). *Latvijas PSR Zinatnu Akad. Vests* 1950, No. 12 (Whole No. 41), 147-60 (Russian summary, 101-2). — The Riga district dolomite marls investigated had the following hydraulic moduli and $\text{CaCO}_3/\text{MgCO}_3$ ratios, resp.: marl I, 1.89, 1/0.987; II, 1.65-2.54, 1/0.947-0.695; III, 1.93-2.37, 1/0.951-0.930. The lime marl (IV) had modulus 1.73-2.23 and contained 72.2-78.2% CaCO_3 . From I, II, and III, satisfactory Roman cements were obtained by baking at 800-850°. Addn. of 1-5% gypsum increased the strength by 10-50% but influenced the hardening time only slightly. IV gave Roman cement upon baking above 1100°. Generally, good cement could be obtained from dolomite marls if they contained over 10% of homogeneously dispersed clay and were baked until the product was left with 4-8% CO_2 content; e.g., heating for 6 hrs. at 760-850° gave best results with piece size 20 X 40 mm. Lime marls were suitable if they contained more than 20%, preferably 25-35%, clay. The mechanism of hardening is discussed on the basis of thermal analysis curves of the products. A. D.

EIDUKS, J.

Chemical Abstracts
May 3, 1954
Glass, Clay Products

3
3
Lead- and boron-free glazes. J. Eiduks and H. Gode.
Latvian PSK Zinidnu Akad. Vēstis 1950, No. 12 (Whole
No. 41), 163-200 (in Russian; Latvian summary, 170).—
Studies were made of the effects of alkali, CaO and MgO,
ZnO and BaO, Fe_2O_3 , P, B_2O_3 , Al_2O_3 and SiO_2 on glazes
fired at 900-1000°. The glazes listed below were prepared
and tested; they are suggested for further study. 0.4
 K_2O + Na_2O , 0.15-0.2 CaO + MgO; 0.4-0.45 BaO +
ZnO, 0.05-0.07 Al_2O_3 , 0.05-0.07 Fe_2O_3 , 1.8 SiO_2 . This
glaze is clear and has good lustre. Thin layer gives little
noticeable craze. The glaze 0.2-0.25 Na_2O , 0-0.1 K_2O ,
0.15-0.2 CaO + MgO, 0.5-0.6 BaO + ZnO, 0.15-0.2
 Al_2O_3 , 0.15 Fe_2O_3 , 3.0-3.2 SiO_2 , 0.4-0.5 B_2O_3 has the same
characteristics as the previous glaze and also withstands a
120° temp. difference. In the absence of BaO and ZnO,
the following glaze is suggested: 0.6-0.7 K_2O + Na_2O ,
0.3-0.4 CaO + MgO, 0.1 Al_2O_3 , 0.5-0.6 Fe_2O_3 , 1.8 SiO_2 ,
0.4-0.5 B_2O_3 . The following glaze will withstand a 100°
temp. difference: 0.4 Na_2O + K_2O , 0.15-0.25 CaO +
MgO, 0.35-0.45 BaO + ZnO, 0.05-0.07 Al_2O_3 , 0.15-0.2
 Fe_2O_3 , 2.0-2.5 SiO_2 , 0.1-0.2 SiF_4 . B. Z. Kamich

1. EIDUKS, J.: VAIVADS, A.: PILSKALNE, A.
2. USSR (600)
4. Latvia - Clay
7. Adsorption properties of various clays of the Latvian S.S.R.
Latv. PSR Zin. Akad. Vestis 2, 1951.
9. Monthly List of Russian Accessions, Library of Congress, January 1953. Unclassified.

1. EYDUKS, J.; VAYVADS, A.; CIRULIS, Fr.
2. USSR 600
4. Paper Industry
7. Fillers for paper from local raw materials, Latv. PSR Zin. Akad. Vestis, No. 9, 1951.
9. Monthly List of Russian Accessions, Library of Congress, April 1953, Uncl.

EX-1000 - Yu. Ya.

5

Bonding materials in gypsum quarry wastes. A. Valzade, L. Eklaks, and B. Hofmanns. *Ibid. Nauk Latv. S.S.R., 1953, 180 pp. (in Russian).*
~~Lat. Philo. (Riga) Separate, 1953, 180 pp. (in Russian).~~
 Wastes from gypsum quarries in the Riga region consist of (A) gypsum high in dolomite, (B) gypsum high in clay, (C) fibrous gypsum, and (D) av. waste rock. Firing of (D) at 170-200° gives a product having the characteristics of "molding plaster." Waste contg. gypsum 20-40, clay 35-50, and dolomite 45-10%, fired at 350-400°, has a tensile strength of 10.5 kg./sq. cm., after setting (7 days). This, fired at 750-850°, gives a cementlike product, in which dolomite acts as activator. Bonding properties are enhanced by the increase of gypsum in waste, but are decreased by firing at temps. higher than 900°. Activators such as 1% Na₂SO₄, 5% CaO, 15% open-hearth furnace slag, burnt dolomite, FeSO₄, and Na₂SO₄ improve bonding properties on firing at 300-700°, but have little effect on firing at temps. higher than 750°. Dissocn. of CaSO₄ for (B) is 0.34% at 800° and 35% at 1100°; for (C), 3.63% at 1300°. X-rays of waste fired at higher temp. indicate a deformation of the CaSO₄ crystal lattice (formation of solid soln.). The bonding properties are due to the hemihydrate, anhydride, and clays, when fired at 150-800°, and to the activated (by MgO) anhydride and hydraulic minerals at 700-900°. (A) gives a product with a longer setting time, when fired at 750-850°; it is easily activated by open-hearth furnace slag, is resistant to moisture, and has the mech. strength of Roman cement. The presence of hydraulic minerals (CaO, Al₂O₃, 2CaO, Fe₂O₃, β-2CaO.SiO₂) gives more stability in humid conditions, but owing to the soln. of gypsum the stability is poor in water. (D) fired at 750-850° is more stable toward humidity and water than is (C). R. S. L.

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EYDUKS, Y

Concretions in Tūjas Middle-Devonian clays. J. Eidūks, V. Dikmane, and K. Karlsons. *Latvijas PSR Zinātņu Akad. Vēstis* 1953, No. 2 (Whole No. 67), 91-7 (Russian summary, 98).—The concretions in the Tūjas (Latvia) Middle-Devonian clays were principally dolomitic. They decreased the firing shrinkage and the bend strength, and increased the water absorption of the products. To obtain satisfactory products, the concretions should be avoided or removed, and the content of the dustlike particles should be below 7% when the sand content is 1% and below 12% when the sand content is below 0.4%. A. D.

2

EYDUKS, Y.

✓ Production of new mortar binders from waste of gypsum mines under industrial conditions. J. Ekdus, A. Valvads, and B. Hofmanis. *Latvian SSR Zinatnu Akad. Vēstis* 1953, No. 4 (Whole No. 69), 91-6 (Russian summary, 96-7).—Waste from gypsum mines contained $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$ 67, dolomite 13.1, and clay 19%. In gypsum stills, at 100-80°, the waste gave a product conforming to specifications for the first grade plaster quality gypsum. In rotation furnace with gases 490-650° in and 150-70° out, a product equivalent to the second grade gypsum was obtained; its properties improved with storage. In the lime oven at 1000-1100°, the product obtained was similar to anhydrite cement, with CaS 1.11, free CaO 14.9, and free MgO 7.5%. The presence of CaS caused nonuniformity of vol. change, which could be amended by storage or by addn. of 0.5-1.0% FeSO_4 . Andrew Dravnieks

2

~~XXXXXXXXXX~~
EYDUKSY.

4

Thermographic and roentgenographic studies of the mineralogical composition of various Latvian Quaternary clays. I. Biduka and A. Vaitys (Inst. Chem., Acad. Sci. Latv. S.S.R., Riga). Latvian P.R. Zinatnu Akad. Vestis 1983, No. 8 (Whole No. 74), 103-10 (Russian summary).—The main constituent of the Latvian Quaternary clays was hydromica (illite) in the Krustpils, Akmistes, and Ozolnieki clays, and another hydromica which was closer to mica than the illite, in the Kalnciemus, Kalkūni, and Brocēni clays. In addition, these clays contained montmorillonite as a transformation product of illite. Accessory minerals were quartz, muscovite, dolomite, hydrogoethite, etc. No kaolinite or halloysite was detected. Andrew Dranovskis.

8 (1)
MST

EYDUKS, I.

1. Thermographic and röntgenographic studies of mineralogical composition of some Latvian Devonian, Triassic, and Jurassic clays. I. Eiduks and A. Vaivads (Inst. Chem., Acad. Sci. Latv. S.S.R., Riga). *Latvian SSR Zinatnu Akad. Vēstis* 1953, No. 10 (Whole No. 76), 125-35 (Russian summary, 136).—Latvian Devonian, Triassic, and Jurassic clays consist mainly of the Illite-type hydromica in various stages of degradation. In Rosien and Pulvernieki Jurassic clays the degradation reached kaolinite (20-5%). In most clays, Na and Mg montmorillonite with rather poorly defined lattice were present in varying amts. The Kengaraga and Saurieši clays belonged to the beidellite type, contg. kaolinite and halloysite (10%). Triassic clays were similar to the Devonian clays. In all clays, hydrated muscovite could be found.

Andrew Dravnieks

KE

①

EYDUKS, Ya.

Thermal expansion coefficients of fired Latvian clays.
J. Ekluks and A. Vaivads. *Latvian PSR Zinātnu Akad.*
Vēstis 1953, No. 12 (Whole No. 77), 131-9 (Russian sum-
mary, 130-40).—The linear thermal expansion coeff. (α)
of Latvian clays fired at 800-1000° was 10×10^{-4} or less.
Quaternary clays had higher α than the Devonian. Pres-
ence of carbonates increased α . In the quartz-bearing
types, α increased proportionally with temp. to 400-450°,
and increased rapidly between 450 and 600°. A. U.

EYDUKS, Ya.

7

Variation of properties of lead-free and boron-free vitreous enamels with the fritting temperature. J. Eydus and A. Latvijas PSR Zinātnu Akad. Vestis 1954, No. 1 (Whole No. 78), 129-38 (Russian summary, 139). The following frits were investigated: Na_2O 0.20, K_2O 0.20, CaO 0.10, MgO 0.03, ZnO 0.30, BaO 0.12, Al_2O_3 0.10, and SiO_2 3.0 moles, and with 0, 0.40, or 0.80 mole F. The best properties were obtained by fritting at 1250-1300°. F decreased the melting temp., alk. of the suspension, and coating temp., but increased the wetting ability of the enamel. The amt. of F left after fritting at 1400° was 0.9-1.1%. The linear thermal expansion coeff. decreased with fritting temp.; this change was larger in the F-bearing enamels. The best enameling temp. decreased by 20-100° with increase in the fritting temp., for the F-bearing types, but did not change in the F-free compns.

Andrew Dravnieks

EXDURS, 1.

Some mineralogical and physicochemical properties of
clays from Cēsis Mārieja. I. Biduks and H. Matisons
(Inst. Chem., Acad. Sci. Latv. S.S.R., Riga). Latvian
PSR Zinātnu Akad. Vēstis 1934, No. 4 (Whole No. 81), 101-
11 (Russian summary, 111-12).—The Devonian clays from
Cēsis Mārieja, Latvia, are purple, green, and brown-red.
The properties of the clays and their fractions are described.
The substance of the finest particles was essentially the same
throughout the formation, but the differences in color and
other properties were traced to the variations in the contents
of iron oxides, mica, montmorillonite, quartz, feldspar, and
accessory trace minerals, in the fractions of the larger par-
ticle sizes. The large inclusions are primarily dolomitic
and seem to have formed simultaneously with the pptn. of the
clays from the geol. lakes. A. Dravnieks

BYDOKS, J.

Ceramic, physical, and chemical properties of some Cedis
Marleja clays. *L. Bolys and H. Matison. Latvian
PSR Zinatnu Akad. Vestis 1954, No. 6 (Whole No. 83),
119-25 (Russian summary, 123-31).*—Cedis Marleja clays
were water-stable after firing at 550-600°. The difference
between the max. firing temp. and clinkering temp. was
80-90° for the carbonate-free clays and less for the carbon-
ate-bearing samples. The basic clay substance, with par-
ticle size below 0.005 mm., was sintered in vac. and showed
a higher vol. increase at a lower temp., compared with the
bulk clay. The soly. in boiling 2N HCl reached a max. at
the firing temp. (750-800°). The dissolved portion con-
tained 27-41% silica and 81-97% alumina. Tech. applica-
tions of these clays are discussed. Andrew Dravnick.

ME

U S S R

Influence of lithium on physicochemical characteristics of low-melting (ceramic) glazes. J. Edinuk and A. Vulyada. *Litvijs PSR Zinatyn Akad. Vestis* 1954, No. 11 (Whole No. 88), 116-29 (in Russian).—Low-melting (ceramic) glazes were prep'd from quartz sand and chemically pure substances. Li₂O amts. up to 7.5% Li₂O was introduced as Li₂CO₃, substituting first on molar basis for Na, K, Ca, and Mg, and then, on wt. % basis, for other elements, starting with a base mixt. (in %): SiO₂ 69.30, Al₂O₃ 11.03, Na₂O 7.0, K₂O 7.08, CaO 2.13, MgO 1.2. The mixt. was fritted at 1300°. Substitution of Li for Na decreased the softening temp. (I) and the temp. (II) at which the liquid phase begins to form. These effects reached a max. at 0.14 mol. % Li₂O. At higher addn., I and II increased again. Substitution of Li for K, Ca, Mg, Si, and Al decreased I and II. The thermal expansion coeff. (III) decreased in substitution of Li for Na to a min. above 3.8 wt. % Li₂O. In substituting Li for K, III decreased to a min. at 1.17-2.67 Li₂O, then, at higher Li content, increased. In substituting Li for Ca, III slightly decreased; for Mg, slightly increased. pH of

over

9. Eideliks etc

suspension was 10-11, and increased with Li content. The ease of grinding increased with substitution of Li for K and Na, decreased with substitution for Ca and Mg. Gloss was the best in mixts. where part of K was substituted by Li; in other substitutions, the gloss changed little. Crystn. (IV) intensified when Li content exceeded 1%. The wetting ability of the molten frits, as measured by the method of contact angles, was generally poor, and did not change by substitution of Li for K, but improved when Li substituted for other components. From considerations of I, II, III, and IV, optimum for Li content was 0.8-1.0%. For articles made of clays contg. 15% carbonates, the best mixt. was (%): SiO_2 70.3, Al_2O_3 12, Na_2O 7.7, K_2O 8.0, CaO 2.2, MgO 1.3, Li_2O 0.58, with III 73×10^{-3} . For feldence three following mixts. are suggested, to be fired at 1020-50°: SiO_2 70.4, 71.2, 73.3; Al_2O_3 12.1, 12.2, 12.6; Na_2O 5.2, 7.8, 8.0; K_2O 7.8, 4.3, 0.0; CaO 2.2, 2.2, 2.2; MgO 1.2, 1.2, 1.3; Li_2O 1.16, 1.17, 2.57. Application of thermographic analysis to detn. of softening, m., and liquidus temp., and crystn. is described.

Andrew Draynieks

LYDUKS, I.

USSR.

1. Increase of the thermal expansion coefficient of ceramic materials. A. Valvada and I. Elduka. *Latvian SSR Zinlatu Akad. Vestis* 1955, No. 1 (Whole No. 90), 139-48 (Russian summary, 148-9).—The influence of various addns. on thermal expansion coeff. (I) of clays was studied at firing temps. 800–1000°, in an attempt to increase I of several Latvian clays from $47-82 \times 10^{-6}$ to $70-88 \times 10^{-6}$, so as to match I of Pb- and Bi-free ceramic glazes. Addn. of 20–30% limestone (II) or dolomite (III) increased I by 37–60%. Na_2CO_3 also increased I; the suggested addn. is 2–3%. Na_2CO_3 also increased the density of the carbonate-free clays if fired at 900°, but in the carbonate-bearing clays at 1000°. I of the natural minerals such as limestone, dolomite, or magnesite was very high ($22-33 \times 10^{-6}$) but rapidly decreased on successive firings, and stabilized at approach to the dissociation temp. It is proposed that this effect explain local glaze failures on the once-fired articles. Viterite, limestone, or dolomite on a percentage basis, were equally efficient in increasing I. Addn. of quartz sand increased I at firing below 900°, but above 900°, max. I was obtained at 5–10% sand. Increases in I resulted also from addn. of $\text{Ca}(\text{OH})_2$, BaCO_3 , and apatite. The following addns. are suggested for best results in increasing I: limestone or dolomite, 10–30%; or Na_2CO_3 , 1–2%; or quartz sand 5–10%; or not more than 2% $\text{Ca}(\text{OH})_2$. A. D.

137-58-6-13020

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 6, p 263 (USSR)

AUTHORS ~~Eyduk, Yu. Ya.~~, Maksimova, O.S., Pauksh, P.G.

TITLE: Titanium Enamels on Cast Iron (Titanovyye emali po chugunu)

PERIODICAL: Uch. zap. Latv. un-t, 1956, Vol 9, pp 169-176

ABSTRACT: The purpose of the study was to obtain white enamel for cast iron pigmented with TiO_2 at a firing temperature $< 800^\circ\text{C}$. Founding of frits was done at a temperature of $1150-1250^\circ\text{C}$, grinding was done in ceramic mills until the $+4900$ mesh/cm² screen residue was 5-10%. The surface of the cast iron was cleaned with wire brushes and emery or by sandblasting (metal-shot blasting). The zone of optimal firing was determined visually after calcination of cast-iron plates with enamel applied during 15 min in a gradient kiln with a variation in temperature from 500 to 1000° . The samples were tested for the degree of whiteness, chemical stability, coefficient of heat expansion, and thermal stability. The contents of the charge and the enamel frits are quoted. High-grade coatings are obtained from R-3 frit containing (in %): SiO_2 48.5, Na_2O 10.7, B_2O_3 7.7, TiO_2 17.3, and Na_2AlF_6 11.9. During the grinding 1%

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Titanium Enamels on Cast Iron

137-58-6-13020

(of frit weight) of NaNO_2 and 1.5% of bentonite should be added to this frit in order to prevent formation of wavy wrinkles in the enamel. The following frit of group VII proved to be the best of the boron-free frits studied: SiO_2 61.34, Na_2O 18.89, K_2O 1.15, MgO 0.52, CaO 3.80, Al_2O_3 5.19, TiO_2 4.29, and CaF_2 4.82. During its grinding 12-15% (of weight of frit) of TiO_2 and 1.5% of bentonite are added in order to obtain a good opaqueness of the enamel. These enamels meet the technical standards relative to thermal stability and mechanical properties and greatly surpass the factory enamel in whiteness and chemical stability. Enamels of various bright colors were obtained on the base of low-melting boron-free frit.

Ts.G.

1. Cast iron--Coatings
2. Enamel coatings--Applications
3. Titanium--Applications

Card 2/2

507/2286

University of Bristol, G. 14,
Chemistry Faculty, 4
Alps, 1977. 291 p. 350 copies printed.

Ms. (this page): A.B. Iyeria'ab, Professor, Doctor of Chemistry; L.E. Lapin', Member of the Academy of Sciences Latvian SSR, Professor, Doctor of Chemistry; G.A. Kozag, Professor, Doctor of Chemistry; Tech. St.: A. Peterson

newcomers; this pool is intended for innovative chemicals and scientists in the commercial industries.

Contents: The book contains 22 articles on organic chemical synthesis and analysis and the physicochemical properties and compositions of ceramic and refractory materials. 16 personalities are mentioned. Figures, tables, and references accompany the articles.

3. Stannous chloride, 2.5 g. and 5.0 g. of sodium
hydroxide in quantitative analysis. The use of sodium

~~Aluminum Oxide~~ Aluminum Oxide by Alumina and Alumina. The luminescence of

and the corrosion of Aluminum in Aluminum sulfate solutions

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Slipsh, J. Properties of Typical Clays of the Latvian SSR 99

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AVAILABLE: Library of Congress

CONCLUSIONS

EYDUK, YU. YA.

LATVIA / Chemical Technology. Ceramics, glass,
cement, materials, concrete.

H

Abs Jour: Ref Zhur-Khimiya, No 12, 1958, 40461.

Author : Eyduk, Yu. Ya.

Inst : Latvian University.

Title : Properties of Low-Baking Gypsum.

Orig Pub: Zinatn. Raksti. Latv. Univ., 1957, 14, 123-154.

Abstract: A relationship between gypsum properties (G) and grinding fineness, heating temperature and others, as well as the nature of the dihydrate structure and granulation of the baked G was established. The presence of medium and fine particles with a low content of particles of less than 0.005 mm of G is being specified as the optimum condition. The beginning of the hardening time is greater than 10 minutes, the temperature interval from

Card 1/4

10

LATVIA / Chemical Technology. Ceramics, glass,
cement, materials, concrete.

H

Abs Jour: Ref Zhur-Khimiya, No 12, 1958, 40461.

Abstract: All modifications of the low-baked G are rapidly hydrated to SH; the further hydration process proceeds unequally, depending on the baking temperature. The strength of pure gypsum at the same w/c is approximately the same. In the rapid dehydration of G at temperatures higher than 300°C (for instance, baking in a suspended state), a soluble A is formed on the surface of the particles, which provides a fast settling of G. Baked G contains β -SH, β -dehydrated SH, a soluble A, dihydrate, and insoluble A. The minimum amount of dihydrate and insoluble A is present in digested gypsum. G obtains the least normal density by baking it in rotating kilns, and the most, by baking it in a suspended state (Leshe's mill).

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SOV/137-58-7-15479

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 7, p 222 (USSR)

AUTHORS: Eyduk, Yu.Ya., Pauksh, P.G., Maksimova, O.S.

TITLE: Influence of Some Technological Factors on the Properties of Covering Enamels on Cast Iron (Vliyaniye nekotorykh tekhnologicheskikh faktorov na svoystva pokrovnykh emaley po chugunu)

PERIODICAL: Zinatn. raksti. Latv. Univ., Uch. zap. Latv. un-t, 1957, Vol 14, pp 221-224

ABSTRACT: On introduction of a small amount of TiO_2 (4.5%) as a separate component or as a titanium flux (Na_2O , SiO_2 , TiO_2) the properties of the enamels investigated did not change from the method of introduction. Introduction of TiO_2 as a separate component simplifies the technique of preparation of frits. Upon substitution of 1% B_2O_3 in the composition of the enamel for 1% SiO_2 the wetting capacity of the enamels is increased considerably and the firing temperature is somewhat lowered. The best milling additive for the Ti enamels investigated is 1-2% of bentonite which has considerably greater binding ability than the

Card 1/2

SOV/137-58-7-15479

Influence of Some Technological Factors (cont.)

usual plastic clays. Too fine a milling of frits contributes to the appearance of the defect known as "korezhina" ("writhing"). The best results were produced when the slip contained 5-12% of 0.05-0.01 mm diam particles. When the slip contains more of such particles the quality of the surface on firing is impaired.

R. A.

1. Enamel coatings--Binders
2. Titanium oxides--Applications
3. Cast iron--Coatings

Card 2/2

Eiduks, J.

4

Physicochemical properties of leadless and boronless pottery glasses containing oxides of barium, zinc, and strontium. A. Ubilo, A. Velivada, and J. Eiduks. *Lettres PSR Science Acad. Vilnius*, 1938, No. 4, 113-22. The lower linear thermal coeff. of expansion of glasses were obtained upon the following ratio of oxides: ZnO:BaO 8:1, ZnO:SrO 1:1, and BaO:SrO:ZnO 1:1:8. The higher temps. of softening of frits were established at the following mol. ratio of oxides: ZnO:BaO 3:1 and ZnO:SrO 1:1. Chem. stability of glasses increases with the increase of ZnO content. During the fritting the formation of two products of liquation was established, one of which contained a large amt. of P compds. and is present in the melt in the form of separate layer or finely dispersed drops. The presence of ZnO aids in the stabilization of emulsion structure. The optimal luster of glasses at the low temp. of deposition was attained at the high content of ZnO in them. Glasses which are deposited at 950-1000° have a good luster and good chem. stability.

T. Cheron

jj

EIDUKS, J. *Y. Y.*

GENERAL

PERIODICALS: VESTIS, No. 5, 1958

EIDUKS, J. Mineralogical properties of nonlead and nonboron pottery glazes containing BaO, ZnO, and SrO. p. 113.

Monthly list of East European Accessions (E AI) LC, Vol. 8, No. 2,
February 1959, Uncl_{ss}.

EIDUKS, J., AND OTHERS.

GENERAL

PERIODICALS: VESTIS, NO. 8, 1958

EIDUKS, J., AND OTHERS. Clays of the Latvian Jurassicsystem. In
Russian. p. 111.

Monthly list of East European Accessions (EEAI) LC, VOL.8, No.2
February 1959, Unclass.

SOV/136-59-5-17/21

AUTHORS: Savin, A.V., and Eyduk, Yu.A.

TITLE: Low-Temperature Sintering of Molybdenum
(Nizkotemperaturnoye spekaniye molibdena)

PERIODICAL: Tsvetnyye metally, 1959, Nr 5, pp 81-84 (USSR)

ABSTRACT: The possibility of obtaining Mo by sintering at 1400 - 1700 °C was investigated. Mo powder reduced at various temperatures (Fig 1), and a hydrogen atmosphere with varying moisture contents were used. The powder was pressed into slabs 12X12X500 mm and heated. The specific weight before and after sintering was found. The compacting pressures used were 4 and 10 T/cm² for fine and coarse powder, giving specific weights of 5.5-6 and 9 g/cm³ respectively. The results of sintering were estimated by the compacting coefficient, (K) i.e. the ratio of the volume of a pore after sintering to the original volume. Table 1 shows the least values of K or the best sintering properties are obtained using Mo powder reduced at 870 °C. With increase in reducing temperature K increases. The effect of moisture content is seen in the first hour of sintering and is less at 1600-1700 °C than at 1400-1500 °C (Figs 1 and 2).

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SOV/136-59-5-17/21

Low-Temperature Sintering of Molybdenum

The rate of oxidation in the first hour can be retarded by addition of 0.1% C to the Mo powder. Above 1500 °C the beneficial effect of the C falls off presumably because the oxidation ability of water vapour also decreases. Table 2 shows the gas content of Mo produced by low temperature sintering is the same as that in Mo produced by conventional methods. The finest grained structure is obtained from fine powder sintered at 1400-1500 °C and is 5-10 μ . At 1600-1700 °C it is 15-20 μ . Moisture has no effect on the grain size in 1-3 hours. Metallographic examination showed that the coarser the powder the slower the recrystallization. Table 3 shows the results of mechanical tests on 2, 0.9 and 0.5 mm Mo wire produced from the low temperature sintered slabs. Fig 3 shows the change in mechanical properties of 0.5 mm diameter wire after tempering for 3 hours at various temperatures. The wire made from

Card 2/3

SOV/136-59-5-17/21

Low-Temperature Sintering of Molybdenum

coarse-grained powder has the highest mechanical properties.

There are 3 figures, 3 tables and 8 references, of which 3 are English, 1 is German and 4 are Soviet.

Card 3/3

15(2)

AUTHORS:

Zebergs, E., Eiduks, J., Reinis, V.

SOV/156-59-1-46/54

TITLE:

Some Methods of Petrographic Research in Application to the Investigation of Glazes (Nekoteryye metody petrograficheskogo issledovaniya v primenenii k izucheniyu glazurey)

PERIODICAL:

Nauchnyye doklady vysshey shkoly. Khimiya i khimicheskaya tekhnologiya, 1959, Nr 1, pp 177 - 180 (USSR)

ABSTRACT:

For the investigation of the interaction between glaze and body polishes were made vertically to the surface of the glaze and investigated in a polarization microscope with a lateral screening of the field of vision. By this method details and flaws that are not noticeable in ordinary light are clearly revealed (Figure). The refraction indices found by means of the immersion method (Table) also numerically proved these flaws. In flawless glazes with a constant course of the refraction index the intensity of the interaction (of the metamorphic layer) between glaze and body cannot be detected. In this case, flat slabs are sawed from the body vertically to the glaze. One side of the slab is polished and put into a 1% solution of rhodamine B for 24 hours. After washing and

Card 1/2

Some Methods of Petrographic Research in Application
to the Investigation of Glazes

SOV/106-99-1-46/54

drying, such polished sections, under a binocular microscope, clearly show different color zones which can easily be measured micrometrically. Some glazes on faience bodies do not reveal any zones even after an application of this method. In this case, the body is covered with only a thin strip of glaze, polished after firing, and superficially stained with rhodamine B. Under the microscope the glaze intrusion into the body can be seen and measured. The microscopic photographs obtained by means of the procedures specified are given. There are 4 figures, 1 table, and 6 references, 4 of which are Soviet.

ASSOCIATION: Kafedra tekhnologii silikatov Latviyskogo gosudarstvennogo universiteta im. Petra Stuchki (Chair of the Technology of Silicates of Latvian State University imeni P. tr Stuchka)

SUBMITTED: June 16, 1958

Card 2/2

EYDUK, Yu.Ya. [Eiduks, J.]; VAYVAD, A.Ya. [Vaivads, A.]; FREYDENFEL'D, E.Zh. [Freidenfeld, E.]

Physicochemical properties of α - and β - calcium sulfate semi-hydrates. Izv.vys.ucheb.sav.; khim.i khim.tekh. 2 no.6:920-925 '59. (MIRA 13:4)

1. Rishskiy politekhnicheskii institut. Kafedra neorganicheskoy khimicheskoy tekhnologii.
(Calcium sulfate)

EYDUKS, J.

13
Wetting of ceramics by glazes in the presence of active agents. J. Eydūks and O. Kukurs. *Latvijas PSR Zinātnu Akad. Vēstis* 1959, No. 8, 83-90.—A pressed cylinder of the glaze contg. the additive was placed on the ceramic surface, heated to the desired temp., and quenched. The contact angle of the drop with the surface was taken as the measure of wetting. Considerable decrease of the angle was observed with NaOH, borax, and H_2SiF_6 from the wet additives, and with NH_4VO_3 , MO_3 and NH_4NO_3 from the dry additives. A. Bechtel

4E2c(4)
1-80(30)

3
4E2b(V)

VAIVADS, A. (Riga); KUKURS, O. (Riga); EIDUKS, J. (Riga)

Thermography of easily fusible glaze. Vestis Latv ak no.9:107-118
'59. (EEAI 9:10)

1. Latvijas PSR Zinatnu akademijs, Kimijas institutuss.
(Glazes)

PAUKSS, P. (Riga); EIDUKS, J. (Riga); BIDERMANIS, L. (Riga)

Study of possibilities of enameling chill-cast iron. Vestis Latv ak
no.11:91-101 '59. (EEAI 9:11)

1. Latvijas PSR Zinatnu akademijs, Kimijas instituts.
(Enamel and enameling) (Cast iron)

PAUKSH, P.[Pauks, P.](Riga); EYDUK, Yu.[Eiduks, J.](Riga); KAMINSKIS, Ya.
[Kaminskis, J.](Riga)

Effect of the preparation method on the properties of fretted
base glaze of type borax, sand. In Russian. Vestis Latv ak no.3:
119-124 '60. (EEAI 10:7)

1. Akademiya nauk Latvyskoy SSR, Institut khimiyi.
(Borax) (Glazes) (Sand)

YEDUK, Ya. [Eiduks, J.](Riga); IEVIN'SH, A. [Ievins, A.](Riga); OZOLS, Ya.
[Ozols, J.](Riga)

Chemical and rational analyses of some typical Latvian SSR clays
and their fractions. In Russian. Vestis Latv ak no.5:97-104
'60. (EEAI 10:7)

1. Akademiya nauk Latvyskoy SSR, Institut khimii.
(Latvia—Clay)

S/730/60/000/002/001/000

AUTHORS: Savin, A. V., Eyduk, Yu. A.

TITLE: The making of a Co W sintered alloy for tool manufacture.

SOURCE: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov.
Sbornik trudov. no.2. Moscow, 1960. Tverdyye splavy. pp.15-23

TEXT: Fundamental parameters that facilitate the making of a compact single-phase alloy with a low gas content are discussed. A suitably heat-treated Co W alloy exhibits outstanding strength and wear- and corrosion-resistance characteristics which render it eminently suitable for use in the shafts of vibratory resistant tools (or instruments) in lieu of steel. W.P. Sykes' phase diagram (Proc. Soc. Steel Treating, Trans., v.21, 1933, 5 //Abstracter's note: See also ibid., p.385//) shows that at the eutectic temperature Co dissolves about 35% W. In an alloy with 25% W, a single-phase β solid solution exists only above 1075°C, whereas below 1075° the alloy consists of two phases, β and ϵ . Precipitation of the ϵ phase in the supersaturated solid solution leads to dispersive hardening of the alloy at $T > 500^\circ$. St. Stolarz (Metal and Production of Cobalt-Tungsten Alloy, v. IX-X, 1953, 298-302 //sic!//) describes a sintering method for the preparation of a 75% (by weight) Co and 25% W alloy, details of which are summarized. The authors

Card 1/4

The making of a Co-W sintered alloy.

S/736/60/000/002/001/0

used ammonium paratungstate (APW) produced by the "Pobeda" factory, and tungsten anhydride (WA) of the hard-alloy plant of the Dzerzhovsk Council of the National Economy. The APW was calcinated to WA at 800°C in a muffle furnace. WA was reduced to W in a H stream in a two-stage tubular furnace 51 mm diam, 1500 mm long. 50-g batches of WA were treated in 10x200-mm reaction boats. In Stage I the boat advanced at 13.3 mm/min, at 650°, in an 800-1000 l/hr H stream, and in Stage II at 10.0 mm/min, at 800°, in a like H stream. The resulting W powder was sifted through a No. 0.112-0.1 (130-150-mesh) sifter and stored in a tightly stoppered glass container. It contained 0.3-0.6 mg/g adsorbed methanol, 0.2-0.3% O; its dry uncompressed weight was 0.9-1.1 g/cm³. The charge was reduced to metallic Co in the same furnace in 120-g batches carried in 10x200 mm iron boats, advancing at 13.2 mm/min at a temperature of 580° and in a 1000 l/hr H stream. The resulting Co powder was sifted through a No. 0.112-0.1 (130-150-mesh) sifter and stored. It contained 0.2-0.5% O, 0.4-0.5 mg/g adsorbed methanol, 0.2-0.3% dry, uncompressed weight: 0.6-0.7 g/cm³. A 15/25 (by weight) Co/W-powder charge was mixed in a 5-liter 180-mm dia porcelain ball mill with 25-mm dia balls; ball weight totaled 1/2 charge weight. However ball weight would have produced hardened shiny Co flakes. The mixture was pressed into 10x10x40 mm rods in a dismantlable steel die at a 3 ton/cm² pressure. The rods were sintered in two stages in an alumin furnace with Mo. Sintering temperature and atmosphere.

Card 2/4

The sintering of a Co-W sintered alloy...

(continued)

time were varied; the H₂ atmosphere had a humidity of 0.1-1.0 mm Hg and a dew-point temperature of 21-30°C. The samples attained a compact metallic appearance, and a fully homogeneous phase β solid solution structure. Under secondary sintering at 1100°C, porosity is negligible (spec. grav. 5.42 g/cm³). At 800°C the spec. grav. is 4.60, at 1100°C 8.59. The effects of various sintering procedures on the structure and density of the resulting β phase are tabulated. Following a preliminary sintering at 800°C the ultimately sintered alloy was free of inclusions. Yet, under identical second sintering, specimens initially sintered at 1100°C contained, as a rule, extraneous inclusions, the composition and character of which unknown. In samples sintered directly at 1100-1300°C without preheating, the structure was completely homogeneous, but their porosity (2-15%) consisted of pre-sintered specimens (0.2-1.5%). The time of pre-sintering (2-30 min, 3-6 hours) did not affect the homogeneity or density of the alloy upon secondary sintering. The gas content of the ultimate products was minimized by a low humidity of the H₂ atmosphere, a low dew-point temperature of the component powders (usually 0-10°C by weight), a low humidity of the H₂ atmosphere, and a long holding time during secondary sintering. The pre-sintering does not produce a significant degassing effect, but the secondary sintering reduces the gas content to 20% or more. Recommendations for the sintering of Co-W powder should not exceed 0.1% and the Co powder 0.5% by weight.

Card 1/1

EYDUK, Yu. [Eiduk, J.] (Riga); PAUKSH, P. [Paukss, P.] (Riga)

Effect of the fineness of admixture grinding on the properties
of fritted prime coat enamels. In Russian. Vestis Latv ak no.5:
105-108 '60. (EEAI 10:7)

1. Akademiya nauk Latvyskoy SSR, Institut khimii.
(Enamel and enameling)

EIDUKS, Julijs; KAININS, Martins; MACEJEVSKA, E., red.; AIZUPIETE, M.,
tekh. red.

[Minerals of the Latvian S.S.R. and their use] Latvijas PSR
derigie izrakteni un to izmantosana. Riga, Latvijas Valsts
izdevnieciba, 1961. 430 p. (MIRA 15:3)
(Latvia--Mines and mineral resources)

EYDUK, Yu.Ya.

Rapid methods for the quality control of glazes and glaze coatings.
Stek. i ker. 19 no.3:32-35 Mr '62. (MIRA 15:3)
(Glazes) (Ceramics--Quality control)

18.1247

1454

28879
S/180/61/000/004/017/020
E073/E535

AUTHORS: Baskin, M.L., Savin, A.V., Tumanov, V.I. and Eyduk, Yu.A. (Moscow)

TITLE: Mutual solubility of copper and molybdenum and certain properties of molybdenum-copper alloys

PERIODICAL: Izvestiya Akademii nauk SSSR. Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1961, No.4, pp.111-114

TEXT: Mo-Cu alloys are extensively used for electric contacts. The authors prepared alloys containing 1.5 to 14% Cu by means of current powder metallurgy methods. Sintering of molybdenum was carried out at 1700°C and the alloys of molybdenum with low contents of copper (1.5 to 10% by weight) were sintered at the same temperature. At lower temperatures, either no sintering took place at all or the material was very porous. The alloy with 14% Cu sintered at 1600°C. The porosity of the produced alloys (determined metallographically) was about 0.6 volume % and that of pure Mo was about 1 volume %. The grain size of the molybdenum phase was approximately the same for all the alloys and also for pure molybdenum, i.e. mainly 25-30 μ. To obtain grains

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Mutual solubility of copper ...

28879
S/180/61/000/004/017/020
E073/E535

of this size molybdenum had to be sintered for a duration almost twice as long as that of the alloys. The properties of the starting materials, Mo and Cu, were as follows: bulk density 1.60 and 1.49 g/cm³, respectively; adsorption of methanol vapours 0.200 and 0.026 mg/g, respectively. The average grain size of the starting powders, Mo and Cu, was 1 to 2 μ . To prevent contamination with iron, the powders were mixed in molybdenum lined mills. The specimens were sintered in molybdenum boats in resistance furnaces with an open molybdenum heater in a hydrogen atmosphere for a duration of one hour and the specimens of pure molybdenum for a duration of two hours. Heat treatment was as follows: heating in a hydrogen atmosphere to 950°C, holding at that temperature for 5 hours and quenching in oil at room temperature. Data on the Mo-Cu alloys are given in Table 2, the column headings from left to right being as follows: Cu, wt.%; specific weight ρ , g/cm³; electric resistance $\rho \times 10^2$ Ohm mm²/m; $\lambda \times 10^6$ 1/deg; phase composition, Mo - denoting Mo-base phase, Cu - denoting copper-base phase (ToX₂ - ditto); lattice parameter kX; Mo-base phase, Cu-base phase. The tabulated electric

Card 2/4

Mutual solubility of copper ...

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S/180/61/000/004/017/020
E073/E535

resistance values are averages from 36 measurements, whereby the maximum error was $\pm 2\%$ and the deviations from the average value did not exceed 0.3%. The coefficient of linear expansion was determined by means of a dilatometer with quartz rods and indicator head in the temperature range 18 to 400°C, the error being within the limits of $\pm 2.5\%$. To determine the influence of admixtures which are important in the industrial manufacture of Mo-Cu alloys, a series of melts were produced containing admixtures of C, Si and SiO₂. Table 3 gives the obtained results for Mo-Cu alloys with 3, 5 and 8% Cu, respectively and the following admixtures in wt. %: 0.05% C, 0.05% Si, 0.10% Si, and 0.50% SiO₂ ($\rho \cdot 10^2$ Ohm mm²/m; a, kX). The influence of nickel (wt. %) on the electric resistance ($\rho \times 10^2$ Ohm mm²/m) of Mo-Cu alloys with 5% Cu was as follows: 0 - 7.10; 0.5 - 10.31; 1.0 - 12.94; 3.0 - 14.92; 5.0 - 15.29. L. G. Grigorovko, A. A. Maksimov and A. A. Cherodinov participated in the experimental work, L. Kh. Pivovarov carried out the X-ray structural analysis and M. N. Nalimova carried out the metallographic investigations. There are 3 figures, 4 tables and

Card 3/2/

Mutual solubility of copper ...

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S/180/61/000/004/017/020
E073/E535

12 references: 4 Soviet and 8 non-Soviet. The English-language references read as follows: Ref.3, C. L. Sargent, J. Amer. Chem. Soc., 1900, v.22, p.783; Ref.7, M. Hansen, Constitution of binary alloys, second edition, New York - Toronto - London, 1958; Ref.12, W. P. Sykes, R. Kent, van Horn and C. M. Tucker, Trans. AIME, 1935, v.117, p.173.

SUBMITTED: July 15, 1960

Table 3

Admixture, wt % Примесей, вес. %	3% Cu		5% Cu		8% Cu	
	$\frac{p \times 10^4}{a \cdot a_{Cu}}$	a, kX	$\frac{p \times 10^4}{a \cdot a_{Cu}}$	a, kX	$\frac{p \times 10^4}{a \cdot a_{Cu}}$	a, kX
—	7.74	8.1397	7.10	8.1397	7.25	8.1397
0.05% C	8.55	8.1393	7.75	—	7.85	8.1395
0.05% Si	—	—	—	—	8.58	—
0.10% Si	—	—	—	—	9.61	—
0.50% SiO ₂	—	—	17.00	8.1375	17.40	—

Card 4/5

PAUKSH, P.[Pauks, P.]; EYDUK, Yu.[Eiduks, J.]

Testing cast iron used in wet-process enameling. Izv. AN Latv.
SSR no.4:77-84 '61. (MIRA 16:1)

1. Institut khimii AN Latvyskoy SSR.

(Enamel and enameling) (Cast iron--Testing)

PAUKSH, P.[Pauks, P.] (Riga); EYDUK, Yu.[Eiduks, J.] (Riga)

Effect of granulometric composition in enamel suspensions on the
properties of wet process ground coat enamels for cast iron. Vestis
Latv ak no.3:77-84 '61. (EEAI 10:9)

1. Akademiya nauk Latvyskoy SSR, Institut khimii.

(Enamel and enameling)

PAUKSH, P.[Pauks, P.](Riga); EYDUK, Yu.[Eiduks, J.](Riga)

Testing of cast iron used for wet process enameling. Vestis Latv
ak no.4:77-84 '61. (EEAI 10:9)

1. Akademiya nauk Latvyskoy SSR, Institut khimii.

(Cast iron) (Enamel and enameling)

S/081/63/000/002/045/088
B156/B144

AUTHORS: Eyduk, Yu. Ya., Skuya, L. A.
TITLE: Determination of the volatility of fluorine in frits and glazes
PERIODICAL: Referativnyy zhurnal. Khimiya, no. 2, 1963, 379-380, abstract 2M111 (Uch. zap. Rizhuk. politekhn. in-t, v.6, 1962, 197-202)

TEXT: The losses of fluorine introduced in the form of NaF have been determined both while fritting glaze mixtures (19.5-31.2%) and while melting them into ceramic substances (17.9-69.2%). It is shown that the losses of F are maximum when the glaze coating is thinnest. The total losses of F when fritting and melting boron-free and lead-free glazes are 25-64%. The moment at which all the F has been distilled can be established by step-by-step titration of the separate fractions in the distillate, and determination of F by the distillation method is thus made more accurate. [Abstracter's note: Complete translation.]

Card 1/1

SVEDE-SHVETS, M.I.; EYDUK, Yu.A.; YENINA, V.A.; VODOP'YANOVA, L.S.;
TRUSHIN, Yu.V.; Prinsipali uchastiye: DZENELADZE, Zh.O.;
ZHUKOVA, Ye.A.; ISAKOVA, Z.S.; PUGACHEVA, V.P.; IGUMNOV, V.Ye.

Thermoelectric characteristics of sintered alloys based on
tungsten and molybdenum. Sbor. trud. TSNNICHM no.30:7-16 '63.
(MIRA 16:10)
(Tungsten-molybdenum alloys--Thermoelectric properties)

EYDUK, Yu. P.; SEDMAL, Yu. N.; BEREZIN, A. Ya.

2

"Concerning the structure of alumosilicophosphate glasses."

report submitted for 4th All-Union Conf on Structure of Glass, Leningrad,
16-21 Mar 64.

EYDUK, Yu.Ya., kand. khim. nauk; KUKUR, O.K., kand. khim. nauk

Defects occurring during the application of easily melted
frit. Stek. 1 ker. 20 no.7:33-36 JI '63. (MIRA 17:2)

1. Rizhskiy politekhnicheskoy institut.

L 12890-66 EWP(e)/EWT(m)/EWP(b) WH

ACC NR: AT6000485 SOURCE CODE: UR/0000/65/000/000/0156/0158

AUTHOR: Eyduk, Yu. Ya.; Sedmal, U. Ya.; Berzin', R. Ya.

ORG: None

TITLE: On the structure of aluminosilicophosphate glasses

SOURCE: Vsesoyuznoye soveshchaniye po stekloobraznomu sostoyaniyu. 4th, Leningrad, 1964. Stekloobraznoye sostoyaniye (Vitreous state); trudy soveshchaniya. Leningrad, Izd-vo Nauka, 1965, 156-158

TOPIC TAGS: lithium glass, aluminophosphate glass, silicate glass, glass property

ABSTRACT: The paper deals with glasses of the three systems $\text{Al}_2\text{O}_3\text{-SiO}_2\text{-P}_2\text{O}_5$, $\text{Li}_2\text{O-Al}_2\text{O}_3\text{-SiO}_2\text{-P}_2\text{O}_5$, and $\text{MgO-CaO-Al}_2\text{O}_3\text{-SiO}_2\text{-P}_2\text{O}_5$. In the first system, studies of the chemical stability, crystallizing tendency, coefficient of linear thermal expansion, softening temperature, and microhardness of the glasses indicate that they consist of the groups $[\text{PO}_4]$, $[\text{AlPO}_7]$, and $[\text{SiO}_4]$, weakly bonded to one another. As the Al_2O_3 content increases, more $[\text{AlPO}_7]$ groups are apparently formed in which P_2O_5 is bound firmly. In the second system, it is postulated that the factor determining glass formation from the standpoint of energy considerations is the similarity between the structure of the vitreous phase and that of the crys-

Card 1/2

L 12890-66

ACC NR: AT6000435

talline phases present in this region. Mineralogical and x-ray diffraction analyses of the crystalline compounds formed showed that crystallization during melting of the glasses involves formation of lithium phosphates and lithium aluminum phosphates. In the third system, the study of physicochemical properties of the glasses indicated that in their crystallization and dielectric properties they are not inferior to aluminum borosilicate glass used in the production of glass fiber, and they are therefore recommended for such use. The glass formation diagrams of the three systems are given. Orig. art. has: 3 figures.

SUB CODE: 07, 11/ SUBM DATE: 22May65

Card

2/2

HW

EYDUK, Yu.Ya. [Eiduks, J.]; BAUMAN, O.F. [Baumans, O.]; RUTIN', I.Ya.

Practices in the use of polymer gypsum. Stroi. mat. 11 no.6:16
Je '65. (MIRA 18:7)

lllll2
S/120/62/000/006/017/029
E192/E382

9.6000
9.3280

AUTHORS: Eydukas, D.Yu. and Barshauskas, K.I.

TITLE: Measuring pulse-generators for investigation of the transient characteristics of semiconductor diodes

PERIODICAL: Pribery i tekhnika eksperimenta, no. 6, 1962,
88 - 94

TEXT: The following method of generating current (voltage) pulses was adopted: first, a voltage pulse of given duration τ is formed and then the required current or voltage pulse is generated. This is done by using a driver pulse source to actuate a circuit for forming the rise time of the pulse; this circuit produces a pulse with a given rise time (5 - 10 ns). Simultaneously, the driver pulse is applied to a delay line and then to a circuit which forms the decay edge of the pulse; this circuit produces a signal of opposite polarity whose position corresponds to the duration of the pulse to be generated. The pulses of opposite polarities determining the leading and trailing edges of the pulse are added and a pulse of required duration is obtained. This is then applied to a forming circuit which produces an output

Card 1/2

Measuring pulse-generators'....

S/120/62/000/006/017/029
E192/E382

current (voltage) pulse of the required amplitude and duration and $\tau_1 = \tau_2 = 5 - 10$ ns. This method was used to design several pulse-current generators producing positive and negative pulses having an amplitude from 1 mA to 5 A and duration of 0.1 - 2 μ s. Similar voltage-pulse generators of 1-2 ohm or 20 - 30 ohm output resistance and with amplitudes of 0.1 - 5 or 1 - 200 V were designed. A double-pulse generator producing a positive current pulse, followed by a negative voltage pulse, or vice versa, and having the same performance parameters as the above generators was also built. The transition time between the top of the current pulse and the maximum amplitude of the voltage pulse in this generator was 7 - 15 ns. The generators were tested experimentally and were used to measure the rise time, storage times and pulse-resistance of a number of semiconductor diodes. The generators could be operated at frequencies up to 200 kc/s. There are 7 figures and 3 tables.

ASSOCIATION: Kaunasskiy, politekhnicheskii institut (Kaunas Polytechnical Institute)

SUBMITTED: January 18, 1962

Card 2/2

1 00001-57 INT(00) DJ/EE
ACC NR: AP0055801

SOURCE CODE: UR/0413/66/000/020/0026/0026

INVENTOR: Eydukevichyus, M. Yu. P.

ORG: None

TITLE: A core for filtration of lubricating oil and diesel fuels. " Class 12,
No. 186972 [announced by the Klaipeda Department of Giprorybflot (Klaypedskoye
otdeleniye)]

SOURCE: Izobreteniya, promyshlennyye obraztzy, tovarnyye znaki, no. 20, 1966, 26

TOPIC TAGS: filter, filtration, paper, diesel fuel, lubricating oil

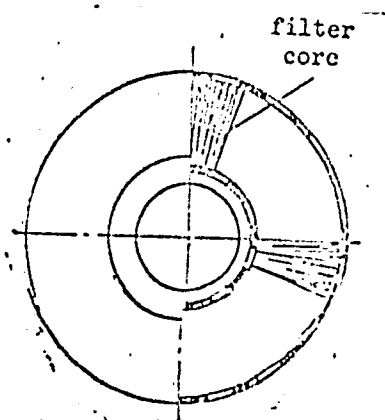
ABSTRACT: This Author's Certificate introduces a core for purification of lubricating
oil and diesel fuel. This element is made from a paper type material in the form of
an accordion pleated strip. The filtration capacity per unit volume of the core is in-
creased by varying the width of the alternating pleats.

Card 1/2

UDC: 662.62:66,067,12.

L 09947-67

ACC NR: AP6035821



SUB CODE: 13, 11/ SUBM DATE: 18Oct65 / ATD PRESS: 5105

ZAYEZDNIY, A.M.; EYDUKYAVICHYUS, G.V.

Abridged representation of signals with the aid of a system of
orthogonal functions. Radiotekhnika 18 no.11:5-12 N '63.
(MIRA 16:12)

1. Deystvitel'nyye chleny Nauchno-tehnicheskogo obshchestva
radiotekhniki i elektrosvyazi imeni Popova.

L 46577-66

ACC NR: AR6016246

SOURCE CODE: UR/0058/65/000/011/H016/H016

AUTHORS: Eydukyavichyus, G.; Kayatskas, A. 2 6

TITLE: Some problems in the application of "optimal bases" for the construction of self organizing systems

SOURCE: Ref. zh. Fizika, Abs. 11Zh121

REF SOURCE: Tr. uchebn. in-tov svyazi. M-vo svyazi SSSR, vyp. 24, 1965, 33-38

TOPIC TAGS: optimal automatic control, self adaptive control, interference immunity

ABSTRACT: The authors consider questions involved in the analysis of noise with the aid of optimal bases, as applied to a self-organizing communication system. Results are presented of experiments on the determination of the interference immunity of signals of various forms when received by an ideal receiver and based on analysis of the noise. The results of the experiments confirm that the optimal bases can find application in self-organizing communication systems. [Translation of abstract]

SUB CODE: 17, 09/

Cord 1/1 hs

MAKARYAVICHYUS, V.I. [Makarevicius, V.]; ZHYUGZEDA, I.I. [Zugzda, J.];
AMBRAZYAVICHYUS, A.B. [Ambrasevicius, A.]; EYIDUKYAVICHYUS, P.I.
[Eidukevicius, P.]; ZHUKAUSKAS, A.A. [Zukauskas, A.]

Speed distribution in the isothermal boundary layer on a plate.
Trudy AN Lit. SSR Ser. B no.3:91-97 '63.

(MIRA 18:3)

1. Institut energetiki i elektrotekhniki AN Litovskoy SSR.

ZHYUGZHDA, I.I. [Ziugzda, J.]; MAKARYAVICHYUS, V.I. [Makarevicius, V.];
SHIANCHYAUSKAS, A.A. [Slanciauskas, A.]; AMBRAZYAVICHYUS, A.B.
[Ambrazevicius, A.]; EYDUKYAVICHYUS, P.I. [Eidukevicius, P.];
ZHUKAUSKAS, A.A. [Zukauskas, A.]

Speed and temperature distribution in the turbulent boundary
layer on a plate. Trudy AN Lit. SSR Ser. B no.3:99-105 '63.
(MIRA 18:3)

1. Institut energetiki i elektrotekhniki AN Litovskoy SSR.

Dependence of the Hydrogen-Carbon Ratio in Liquid Fuel Upon Its Average Specific Gravity. B. R. Eldus. *UOP Library Bulletin of Abstracts*, v. 21, Nov. 27, 1946, p. 191. Abstract from *Journal of Applied Chemistry* (U.S.S.R.), v. 18, 1945, p. 548-555.

952 organic compounds with specific gravities ranging from 0.6 to 1.2 were studied in order to determine above relationship. An equation was derived for characterization of crude oils and oils from coal and peat. Since the H/C ratio is an index of thermal stability and of suitability for engine fuel use, above relationship should be of value in quick estimation of these characteristics. Similar equations were derived for paraffins and naphthenes.

EIDUS, B. R.

2574. NATURE OF DEPENDENCE OF ELEMENTARY COMPOSITION OF PEAT TAR ON SPECIFIC GRAVITY. Eidus, B.R. (J. Appl. Chem., (U.S.S.R.), 1945, 18, 556-63). A relationship between elementary composition and specific gravity of peat tar was shown to exist by the method of arithmetic means. With increase of d. from 0.6 to 1.7, the C content drops linearly from 80% to 34% H content drops linearly from 12% to 1%, O content varies only from 16.3 to 19.9%. The following empirical equations were obtained: $\%C = 113.22 - 46.25d$ and $\%H = 22.39 - 12.6d$.

C.A.

EYDUS, G. R.

Chemical Abst.
Vol. 48 No. 6
Mar. 25, 1954
Cellulose and Paper

The processing of wood tars. B. K. Eldus. *Dereob-
pererabatyayushchaya i Lesokhim. Prom.* 2, No. 11, 15-16
(1953).—The thermochem. stabilities of wood-tar (I) dis-
tillates was improved by distg. over comminuted wood (II)
or charcoal (III). I from slash (IV) and pine holes (V) and
stumps (VI) was pyrolyzed in a 2.5-l. retort: the pyrolysis
time (in min.) (VII), temp. (VIII), yield (IX) of III after
pyrolysis as % of II, yield of I as % of original I (X), and d.
(XI) of III were 280, 460°, 45, 75, and 0.410 for the pyrolysis
of IV (1 part) over II (1 part, 2 × 1 × 1 cm.); 270, 470°,
40, 80, and — for the pyrolysis of V (1 part) over II (1 part);
270, 470°, 35, 75, and 0.270 for the pyrolysis of VI (1 part)
over II (1 part); and 240, 480°, 29, 8, and 0.250 for the py-
rolysis of II alone. VII, VIII, and X for the pyrolysis of V
(2.5 parts) over III (1 part) were 270, 470°, and 70; and for
the pyrolysis of VI (2.5 parts) over III (1 part) were 270, 470°
and 68. The various I were fractionated: the d., sapon.
no. (XII) in mg./g., acid no. (XIII) in mg./g., % C₁₀-insol.
material, yield of fractions b. to 130°, 130-230° (A), 230-
70° (B), 270-300° (C), and above 300° (D), and the sum of
residue and losses were: for IV, 1.103, 19.0, 8.0, 21.5, 7.8,
9.8, 10.3, 10.2, 21.8, and 28.8; for IV after pyrolysis over
II, 1.030, 10.0, 6.0, 8.4, 6.0, 13.7, 17.7, 8.0, 45.0, and 9.4;
for V, 1.075, 14.5, 8.0, 23.0, 13.0, 18.5, 8.0, 4.8, 45.1, and
15.8; for V pyrolyzed over II, 1.030, 6.4, 3.9, 4.6, 10.0, 11.4,
10.0, 7.0, 45.0, and 11.0; for V pyrolyzed over III, 0.995,
25, 18, 0.3, 7.5, 8.5, 9.0, 6.0, 63.0, and 0.0; for VI, 1.065,
13.0, 9.0, 8.5, 3.0, 7.8, 6.5, 6.9, 67.0, and 8.8; for VI after
distn. over II, 1.015, 8.5, 4.5, 1.5, 5.0, 12.0, 11.8, 6.5, 56.0,
and 8.0; and for VI after distn. over III, 0.990, 35, 12, 0.5,
8.0, 15.0, 8.0, 7.0, 63.0, and 4.0. XII, XIII, and the con-
tent of phenols in A-D from V were 130, 73, and 65; 71, 43,
and 60; 70, 25, and 40; and 27, 13, and 25; in A-D from V
after pyrolysis over II were 115, 65, and 50; 67, 31, and 50;
57, 27, and 40; and 10, 7, and 30; and in A-D from V after
pyrolysis over III were 90, 63, and 45; 21, 25, and 40; 35,
18, and 34; and 6, 1, and 7; resp. *Int. Lab. Konyas*

EYDUS, B.R.

Motor oil from wood tars. H. R. Hahn. *Proc. Am. Chem. Soc.* 57, 1935, 1414-1415. A study was made of the prepn. of a lubricating oil for internal-combustion engines from wood tars (1) from tar-pine trees. The lubricating oils tested were obtained by (1) distn. of 1 over wood charcoal to increase its thermal stability, (2) distn. of 1 over wood, and (3) the product of 2 purified with Al_2O_3 . 1, the product of 2, the product of 3, the product of 3 treated with $\text{Ba}(\text{OH})_2$, the product of 1, and a standard tractor lubricating oil (H) had the following amt. of pour-point-increase (°C) at 100, 200, 300, 400, 500, and 600° and the following relative rates of oxidation (wt.-%) at 100, 200, 300, 400, 500, and 600°. Material from 1 showed no oxidation; pour-point-increase to crystallize than did that from 2. Materials from 2 and 3, material from 3 treated with $\text{Ba}(\text{OH})_2$, and H had the following viscosity (centistokes) at 50°: 2.0, 2.5, 3.0, 3.5, 4.0, and at 100°: 1.0, 1.5, 2.0, 2.5, 3.0, 3.5, and 4.0; H had pour-point-increase of 10, 15, 16, 16.5, and 17°; and congealing point was -14, -15, -16, -16, and -17°. Material from 3 treated with $\text{Ba}(\text{OH})_2$ was found satisfactory when used in a 3-horsepower, 2200-c.c.m. engine.

John Edgar Kroy

Eidua, D. M. On a mixed problem of the theory of elasticity. Doklady Akad. Nauk SSSR (N.S.) 76, 181-184 (1951) (Russian)

Consider a finite domain Ω in three-dimensional (x_1, x_2, x_3) -space, with a piecewise smooth boundary Γ which consists of three parts $\Gamma_1, \Gamma_2, \Gamma_3$. A certain mixed problem of the theory of elasticity consists in the determination of the displacement vector u , which satisfies the equation

$$\mu \Delta u + (\mu + \lambda) \operatorname{grad} \operatorname{div} u + f = 0$$

in Ω , and also the following boundary conditions

$$u|_{\Gamma_1} = 0, \quad u_n|_{\Gamma_2} = 0, \quad t|_{\Gamma_3} = 0, \quad t|_{\Gamma_1} = 0,$$

where u and τ denote normal and tangential components, respectively, and t is the stress vector. Let D denote the class of all functions $u = (u_1, u_2, u_3)$ with continuous first partial derivatives in Ω , and such that

$$H(u) = \int_{\Omega} \sum_{i,j=1}^3 u_i \tau_{ij} d\Omega < \infty, \quad D(u) = \int_{\Omega} \sum_{i,j=1}^3 \left(\frac{\partial u_i}{\partial x_j} \right)^2 d\Omega < \infty.$$

Further, let D_1 denote the subset of D consisting of all functions u satisfying $u|_{\Gamma_1} = 0$. Introduce a norm in D , by means of the definition

$$\|u\| = [H(u) + D(u)]^{1/2},$$

and let D_1 be the closure (completion) of the space D_1 with respect to this norm. According to S. G. Mihlin [Direct Methods in Mathematical Physics, Moscow-Leningrad, 1950] in order to solve the above mixed problem one need only establish that there exist positive numbers α and β such that, for any u in D_1 , the following two inequalities hold:

$$(1) \quad H(u) \leq \alpha D(u),$$

$$(2) \quad D(u) \leq \beta H(u),$$

where

$$D(u) = \int_{\Omega} \sum_{i,j=1}^3 \left(\frac{\partial u_i}{\partial x_j} \right)^2 d\Omega, \quad H(u) = \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right).$$

Inequality (1) was proved by S. L. Sobolev [Mat. Sbornik N. S. 2, 4), 467-500 (1937)]. Using results of K. O. Friedrichs [Ann. of Math. (2) 48, 441-471 (1947); these Rev. 9, 255], the present author proves the inequality (2).

J. B. Diaz (College Park, Md.)

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Source: Mathematical Reviews,

Vol 13 No.5

EYDUS, D.M.
July 1954

2120. Stets, B. M. On the solution of boundary problems by the method of finite differences (in Russian), Dokl. Akad. Nauk SSSR (N.S.) 83, 194-194, 1953.

The Dirichlet boundary-value problem has been dealt with by the method of finite differences by L. A. Lyusternik (Mat. zhurnik 33, 173-204, 1933); L. G. Prigorskii (Dop. matem. Nauk 2, 161-170, 1941); R. Courant, K. Friedrichs, and H. Lewy (Math. Ann. 100, 32-74, 1928). In the present paper, other boundary-value problems for the elliptic equation

$$L u = \sum_{i,j=1}^n \frac{\partial}{\partial x_i} \left(a_{ij}(x) \frac{\partial u}{\partial x_j} \right) = f(x), \quad a_{ij} = a_{ji}$$

are treated by the method of finite differences. Particular attention is given to the boundary-value problem where the boundary condition is

$$P u = \sum_{i,j=1}^n a_{ij} \frac{\partial u}{\partial x_i} \cos(\nu, x_j) = 0$$

It is remarked that a similar procedure is applicable to mixed boundary problems and eigenvalue problems for the same operator L .

Journal of Mathematical Analysis

J. B. Diaz, USA

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EYDUS, D. M.

USSR/Mathematics - Eigenfunctions

21 Mar 52

"Continuous Dependence of Eigenfunctions on Region," D.M. Eydus

"Dok Ak Nauk SSSR" Vol 83, No 3 pp 365-367

Considers a finite region O with boundaries G in a space of variables x_m ; and the problem concerning the eigenvalues of the elliptic-type operator $Lu = (d/dx_i) (a_{ij} du/dx_j)$ (ij -summed, 1 to m) for the boundary condition $u|_G = 0$. Submitted by Acad V.I. Smirnov 21 Jan 52.

227T53

EYDUS P.M.

Applied Mechanics Reviews
Vol. 7 No. 4
Apr. 1954
Theoretical and Experimental Methods

925. Eidus, D. M., Estimate of the modulus of eigenfunc-
tions (in Russian), *Doklady Akad. Nauk SSSR* (N.S.), 66, 6, 913
914, June 1953

Paper deals with eigenvalues λ , and normalized characteristic functions u , of the Helmholtz equation $\Delta u + \lambda u = 0$ in a finite region Ω of n -dimensional space and not zero values at the boundary Γ . In this case it is known that $|u| \leq c\lambda^k$ where $k = (n/4) + 1$ and c is constant.

Author establishes this inequality also for $k = n/4$ and, for arbitrary part Ω_0 of Ω , lying within Ω , he gives the exactness of the estimate mentioned above, up to the value $k = (n/4) + 1$. In this case, however, the number c depends upon Ω_0 .

Paper is of mathematical character, but the results have importance in the advanced theory of wave motion and in other fields of mathematical physics. A. A. V. (in Russian)

for 1K

Eydus, D.M.
USSR/Mathematics - Elasticity Theory

FD-829

Card 1/1 : Pub. 64 - 4/10

Author : Eydus, D. M. (Leningrad)
~~USSR/Mathematics - Elasticity Theory~~

Title : The contact problem of elasticity theory

Periodical : Mat. sbor., 34(76), 429-440, May-Jun 1954

Abstract : The problem examined is that of finding in a bounded region in three-dimensional space a displacement vector with projections on the coordinate axes which satisfies a certain equation and three boundary conditions. The author proves five theorems on inequalities using in the proofs lemmas developed earlier in the article.

Institution : --

Submitted : December 18, 1952

Eydus, D.M.

USSR/Mathematics - Boundary problems

Card 1/1 Pub. 22 - 6/60

Authors : Eydus, D. M.

Title : ~~Mathematical problems of the theory of boundary value problems~~
The boundary problem of equation $\Delta u + \lambda^2 u = 0$

Periodical : Dok. AN SSSR 100/4, 631-633, Feb 1, 1955

Abstract : A solution is sought for equation: $\Delta u + \lambda^2 u = 0$. A solution is first considered for the above equation under the following boundary conditions: $u|_S = 0$. Then, the boundary conditions $u|_S = \psi$, are used assuming that $\psi(x)$ is a continuous function over surface S. The author recommends expanding the function ψ along its eigen functions θ_m : $\psi = \sum_{m=1}^{\infty} (\psi, \theta_m) \theta_m$, then a solution of the boundary problem $u(x)$, where $x \in \Omega$, can be found and expressed as follows:

$$u(x) = \sum_{m=1}^{\infty} \frac{(\psi, \theta_m)}{\lambda_m} \int_S \frac{\sin \lambda_m r_{xy}}{r_{xy}} \theta_m(y) dS_y.$$

Institution : Leningrad Institute of Aircraft Instrument Construction

Presented by: Academician V. I. Smirnov, November 17, 1954

EYDUS D M

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math

2

Eidus, D. M. On the existence of the normal derivative of the solution of the Dirichlet problem. Vestnik Leningrad Univ. 11:1 (1966), no. 1, 47-50. (Russian)
 Let Ω be a finite region in E_n with a piecewise-smooth boundary S . Let φ be a function defined on S . Let q be a function defined on S by a continuous parameterization. The existence of the normal derivative of functions continuous on S is proved. The norm is defined by

$$\|q\|^2 = \int_S (q^2 + \text{grad}_S^2 q) dS,$$

where $\text{grad}_S \varphi$ is the surface gradient of φ , the norm in $D(S)$. Let $W_2^1(S)$ denote the space obtained by the closure of the linear manifold $L(S)$ with respect to the norm $\|q\|$. It is shown that if the function $\varphi \in W_2^1(S)$, then the harmonic function u in Ω coincides with φ on S has the property that its normal derivative $\frac{\partial u}{\partial n}$ exists almost everywhere on S . (Received April 11, 1966)

1966a:35B30, 35B45, 35B65, 35B66, 35B67, 35B68, 35B69, 35B70, 35B71, 35B72, 35B73, 35B74, 35B75, 35B76, 35B77, 35B78, 35B79, 35B80, 35B81, 35B82, 35B83, 35B84, 35B85, 35B86, 35B87, 35B88, 35B89, 35B90, 35B91, 35B92, 35B93, 35B94, 35B95, 35B96, 35B97, 35B98, 35B99, 35C00, 35C01, 35C02, 35C03, 35C04, 35C05, 35C06, 35C07, 35C08, 35C09, 35C10, 35C11, 35C12, 35C13, 35C14, 35C15, 35C16, 35C17, 35C18, 35C19, 35C20, 35C21, 35C22, 35C23, 35C24, 35C25, 35C26, 35C27, 35C28, 35C29, 35C30, 35C31, 35C32, 35C33, 35C34, 35C35, 35C36, 35C37, 35C38, 35C39, 35C40, 35C41, 35C42, 35C43, 35C44, 35C45, 35C46, 35C47, 35C48, 35C49, 35C50, 35C51, 35C52, 35C53, 35C54, 35C55, 35C56, 35C57, 35C58, 35C59, 35C60, 35C61, 35C62, 35C63, 35C64, 35C65, 35C66, 35C67, 35C68, 35C69, 35C70, 35C71, 35C72, 35C73, 35C74, 35C75, 35C76, 35C77, 35C78, 35C79, 35C80, 35C81, 35C82, 35C83, 35C84, 35C85, 35C86, 35C87, 35C88, 35C89, 35C90, 35C91, 35C92, 35C93, 35C94, 35C95, 35C96, 35C97, 35C98, 35C99, 35D00, 35D01, 35D02, 35D03, 35D04, 35D05, 35D06, 35D07, 35D08, 35D09, 35D10, 35D11, 35D12, 35D13, 35D14, 35D15, 35D16, 35D17, 35D18, 35D19, 35D20, 35D21, 35D22, 35D23, 35D24, 35D25, 35D26, 35D27, 35D28, 35D29, 35D30, 35D31, 35D32, 35D33, 35D34, 35D35, 35D36, 35D37, 35D38, 35D39, 35D40, 35D41, 35D42, 35D43, 35D44, 35D45, 35D46, 35D47, 35D48, 35D49, 35D50, 35D51, 35D52, 35D53, 35D54, 35D55, 35D56, 35D57, 35D58, 35D59, 35D60, 35D61, 35D62, 35D63, 35D64, 35D65, 35D66, 35D67, 35D68, 35D69, 35D70, 35D71, 35D72, 35D73, 35D74, 35D75, 35D76, 35D77, 35D78, 35D79, 35D80, 35D81, 35D82, 35D83, 35D84, 35D85, 35D86, 35D87, 35D88, 35D89, 35D90, 35D91, 35D92, 35D93, 35D94, 35D95, 35D96, 35D97, 35D98, 35D99, 35E00, 35E01, 35E02, 35E03, 35E04, 35E05, 35E06, 35E07, 35E08, 35E09, 35E10, 35E11, 35E12, 35E13, 35E14, 35E15, 35E16, 35E17, 35E18, 35E19, 35E20, 35E21, 35E22, 35E23, 35E24, 35E25, 35E26, 35E27, 35E28, 35E29, 35E30, 35E31, 35E32, 35E33, 35E34, 35E35, 35E36, 35E37, 35E38, 35E39, 35E40, 35E41, 35E42, 35E43, 35E44, 35E45, 35E46, 35E47, 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35K20, 35K21, 35K22, 35K23, 35K24, 35K25, 35K26, 35K27, 35K28, 35K29, 35K30, 35K31, 35K32, 35K33, 35K34, 35K35, 35K36, 35K37, 35K38, 35K39, 35K40, 35K41, 35K42, 35K43, 35K44, 35K45, 35K46, 35K47, 35K48, 35K49, 35K50, 35K51, 35K52, 35K53, 35K54, 35K55, 35K56, 35K57, 35K58, 35K59, 35K60, 35K61, 35K62, 35K63, 35K64, 35K65, 35K66, 35K67, 35K68, 35K69, 35K70, 35K71, 35K72, 35K73, 35K74, 35K75, 35K76, 35K77, 35K78, 35K79, 35K80, 35K81, 35K82, 35K83, 35K84, 35K85, 35K86, 35K87, 35K88, 35K89, 35K90, 35K91, 35K92, 35K93, 35K94, 35K95, 35K96, 35K97, 35K98, 35K99, 35L00, 35L01, 35L02, 35L03, 35L04, 35L05, 35L06, 35L07, 35L08, 35L09, 35L10, 35L11, 35L12, 35L13, 35L14, 35L15, 35L16, 35L17, 35L18, 35L19, 35L20, 35L21, 35L22, 35L23, 35L24, 35L25, 35L26, 35L27, 35L28, 35L29, 35L30, 35L31, 35L32, 35L33, 35L34, 35L35, 35L36, 35L37, 35L38, 35L39, 35L40, 35L41, 35L42, 35L43, 35L44, 35L45, 35L46, 35L47, 35L48, 35L49, 35L50, 35L51, 35L52, 35L53, 35L54, 35L55, 35L56, 35L57, 35L58, 35L59, 35L60, 35L61, 35L62, 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35N06, 35N07, 35N08, 35N09, 35N10, 35N11, 35N12, 35N13, 35N14, 35N15, 35N16, 35N17, 35N18, 35N19, 35N20, 35N21, 35N22, 35N23, 35N24, 35N25, 35N26, 35N27, 35N28, 35N29, 35N30, 35N31, 35N32, 35N33, 35N34, 35N35, 35N36, 35N37, 35N38, 35N39, 35N40, 35N41, 35N42, 35N43, 35N44, 35N45, 35N46, 35N47, 35N48, 35N49, 35N50, 35N51, 35N52, 35N53, 35N54, 35N55, 35N56, 35N57, 35N58, 35N59, 35N60, 35N61, 35N62, 35N63, 35N64, 35N65, 35N66, 35N67, 35N68, 35N69, 35N70, 35N71, 35N72, 35N73, 35N74, 35N75, 35N76, 35N77, 35N78, 35N79, 35N80, 35N81, 35N82, 35N83, 35N84, 35N85, 35N86, 35N87, 35N88, 35N89, 35N90, 35N91, 35N92, 35N93, 35N94, 35N95, 35N96, 35N97, 35N98, 35N99, 35O00, 35O01, 35O02, 35O03, 35O04, 35O05, 35O06, 35O07, 35O08, 35O09, 35O10, 35O11, 35O12, 35O13, 35O14, 35O15, 35O16, 35O17, 35O18, 35O19, 35O20, 35O21, 35O22, 35O23, 35O24, 35O25, 35O26, 35O27, 35O28, 35O29, 35O30, 35O31, 35O32, 35O33, 35O34, 35O35, 35O36, 35O37, 35O38, 35O39, 35O40, 35O41, 35O42, 35O43, 35O44, 35O45, 35O46, 35O47, 35O48, 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35P92, 35P93, 35P94, 35P95, 35P96, 35P97, 35P98, 35P99, 35Q00, 35Q01, 35Q02, 35Q03, 35Q04, 35Q05, 35Q06, 35Q07, 35Q08, 35Q09, 35Q10, 35Q11, 35Q12, 35Q13, 35Q14, 35Q15, 35Q16, 35Q17, 35Q18, 35Q19, 35Q20, 35Q21, 35Q22, 35Q23, 35Q24, 35Q25, 35Q26, 35Q27, 35Q28, 35Q29, 35Q30, 35Q31, 35Q32, 35Q33, 35Q34, 35Q35, 35Q36, 35Q37, 35Q38, 35Q39, 35Q40, 35Q41, 35Q42, 35Q43, 35Q44, 35Q45, 35Q46, 35Q47, 35Q48, 35Q49, 35Q50, 35Q51, 35Q52, 35Q53, 35Q54, 35Q55, 35Q56, 35Q57, 35Q58, 35Q59, 35Q60, 35Q61, 35Q62, 35Q63, 35Q64, 35Q65, 35Q66, 35Q67, 35Q68, 35Q69, 35Q70, 35Q71, 35Q72, 35Q73, 35Q74, 35Q75, 35Q76, 35Q77, 35Q78, 35Q79, 35Q80, 35Q81, 35Q82, 35Q83, 35Q84, 35Q85, 35Q86, 35Q87, 35Q88, 35Q89, 35Q90, 35Q91, 35Q92, 35Q93, 35Q94, 35Q95, 35Q96, 35Q97, 35Q98, 35Q99, 35R00, 35R01, 35R02, 35R03, 35R04, 35R05, 35R06, 35R07, 35R08, 35R09, 35R10, 35R11, 35R12, 35R13, 35R14, 35R15, 35R16, 35R17, 35R18, 35R19, 35R20, 35R21, 35R22, 35R23, 35R24, 35R25, 35R26, 35R27, 35R28, 35R29, 35R30, 35R31, 35R32, 35R33, 35R34, 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Eydus, D. M.

USSR/ Mathematics

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Authors : Eydus, D. M.

Title : Evaluations of Green function derivatives

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Abstract : A proof is presented that the derivatives of Green's function may be evaluated by the same principle which has been used in evaluating derivatives of potential of a simple layer of the density satisfying Lipshits' conditions. Three references: 2 USSR and 1 Swiss. (1919-1953).

Institution : Leningrad Institute of Aviation Instrument Manufacture

Presented by: Academician V. I. Smirnov, October 7, 1955

EJDUS, D.M.

SUBJECT USSR/MATHEMATICS/Differential equations CARD 1/1 PG - 314
 AUTHOR EJDUS D.M.
 TITLE Some inequations for eigenfunctions.
 PERIODICAL Doklady Akad. Nauk 107, 796-798 (1956)
 reviewed 10/1956

Let λ_n be the eigenvalue with the number n of the equation $\Delta u + \lambda u = 0$ in the m -dimensional finite region Ω with the boundary surface S for the boundary value condition $u|_S = 0$. Let u_n be the corresponding eigenfunction which is normalized by the condition $\int_{\Omega} u_n^2 d\Omega = 1$. Let D^k be the operation of the k -times differentiation with respect to the coordinates of the point x . Under the assumption that for $k = 0$ the surface S is $(k+1)$ -times continuously differentiable, $k \geq 1$, the author proves the inequation

$$|D^k u_n(x)| \leq c_k \lambda_n^{\frac{m-1}{4}} (\ln \lambda_n)^{1/2},$$

which in Ω is valid for all n for which $\lambda_n > 1$. Some further similar inequations are mentioned.

AUTHOR: Eydus, D.M. (Leningrad) SOV/39-45-4-4/7
 TITLE: Inequations for the Green's Function (Neravenstva dlya funktsii Grina)
 PERIODICAL: Matematicheskiy sbornik, 1958, Vol 45, Nr 4, pp 455-470 (USSR)
 ABSTRACT: Let Ω be a finite open domain of the three-dimensional space, let S be the boundary of Ω . The author considers the Green's function $G(x,y)$ of the Laplace operator for the Dirichlet problem in Ω . It is

$$G(x,y) = \frac{1}{4\pi r_{xy}} + g(x,y),$$

where $g(x,y)$ is the regular part of $G(x,y)$. Let $Dg(x,y)$ and $D^2g(x,y)$ respectively, denote the first and second, respectively, derivative of $g(x,y)$ with respect to one of the variables. Let

$$g_1(x,y) = \frac{1}{8\pi^2} \int_S \frac{1}{r_{xt}} \frac{\partial}{\partial n_t} \left(\frac{1}{r_{ty}} \right) ds_t,$$

where n_t is the outer normal of S in the point t . Under certain

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Inequations for the Green's Function

SOV/39-45-4-4/7

assumptions on S (it has to be a Lyapunov-surface with exponents λ)
the author proves the inequations

$$|g_1(x,y)| \leq c_1 \frac{1}{r_{xy}}, \quad |g(x,y) - g_1(x,y)| \leq c_2 r_{xy}^{\lambda-1}$$

and furthermore

$$|Dg_1(x,y)| \leq c_3 r_{xy}^{-2}, \quad |D(g - g_1)| \leq c_4 (\lambda') r_{xy}^{\lambda'-2}, \quad \lambda' < \lambda$$

$$|D^2 g_1(x,y)| \leq c_5 r_{xy}^{-3}, \quad |D^2(g - g_1)| \leq c_6(\varepsilon) r_{xy}^{-2-\varepsilon},$$

where in the last inequations $\varepsilon > 0$ may be arbitrary, but it has
to be $\lambda = 1$ and some further difficult demands are to be satisfied
by S.

From these inequations there follows the inequation

$$|Dg(x,y)| \leq c r_{xy}^{-2}$$

announced in an earlier paper of the author [Ref 2].

There are 3 references, 2 of which are Soviet, and 1 Polish.

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1. Topology 2. Functions - Theory

Card 2/2